
Introduction

Purpose

- To provide an overview of the main considerations when selecting a PowerStor supercapacitor.

Objectives

- Enable engineers to make a basic product selection using only four circuit parameters
- Review the effects of temperature and aging on supercapacitor performance
- Look at the required precautions when connecting supercapacitors in series
- Explain inflow current, self leakage and leakage current

Supercapacitor Applications

- **Pulse**
 - High current for short duration
- **Bridge or Hold-up Power**
 - High current for short duration, followed by ultra-low current, sleep mode for longer duration
- **Main**
 - Lower current or short duration
- **Memory Backup**
 - Ultra-low current, sleep mode for long duration



Parameters Required for Supercapacitor Selection

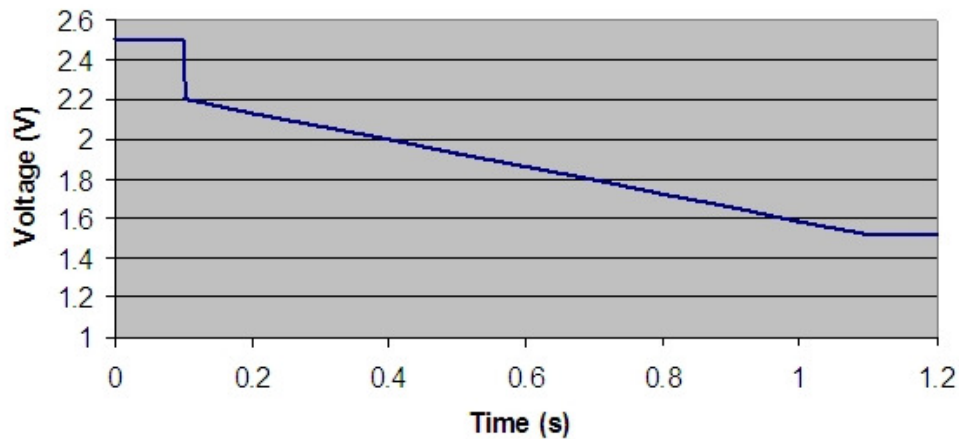
Four Basic Selection Parameters:

- Nominal Operating Voltage
- Minimum Allowable Voltage (circuit drop-out voltage)
- Average Capacitor Discharge Current
- Duration of Required Hold-up or Current Pulse

Additional Selection Criteria:

- Operating Temperature Range
- Required Operating Life

Capacitor Discharge Voltage



Calculating Minimum Capacitance

Minimum capacitance can be calculated using the equation:

$$i = C \cdot dv / dt$$

Where, i is the discharge current, C is the capacitance, dv is the change in voltage and dt is the duration of the discharge. From this we get:

$$C = (i \cdot dt) / dv$$

For example, a system has a nominal voltage of 2.5V and a drop out voltage of 2.0V. The system must continue to operate for 5 seconds after a mains fail and has an average current demand of 0.5A. In this case:

$$C = (0.5A \times 5s) / (2.5V - 2.0V) = 5 \text{ Farad}$$

Calculating Maximum ESR

Maximum ESR can be calculated using the equation:

$$V = I \cdot R$$

Where, I is the discharge current, R is the ESR and V is the voltage drop. From this we get:

$$R = V / I$$

Using the same example of nominal voltage of 2.5V, drop out voltage of 2.0V, 5 seconds hold up time and average current demand of 0.5A:

$$R = (2.5V - 2.0V) / 0.5A = 1 \text{ Ohm}$$

Capacitor Selection

So we are looking for a capacitor with capacitance $>5\text{F}$ and $\text{ESR} < 1 \text{ Ohm}$. Looking at the PowerStor supercapacitor data sheets we find that the B1030-2R5685-R gives 6.8F with $0.1 \text{ Ohm ESR @ } 1\text{kHz}$.

For a DC discharge the specified ESR must be multiplied by 1.5.

So, for the given example, the voltage drop using the B1030-2R685-R will be:

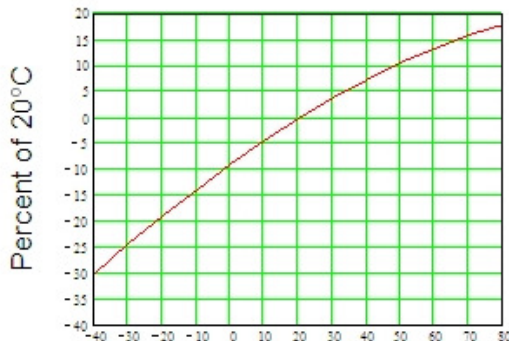
$$\begin{aligned} &= i \cdot (R + t/C) = 0.5\text{A} \times (0.15\Omega + 5 \text{ s} / 6.8 \text{ F}) \\ &= 0.443\text{V} \end{aligned}$$

This meets the basic requirements of the application for a voltage drop of $< 0.5\text{V}$.

Additional Selection Criteria

Operating Temperature Range:

Percent Capacitance
Change Over
Temperature Range



Temperature - C

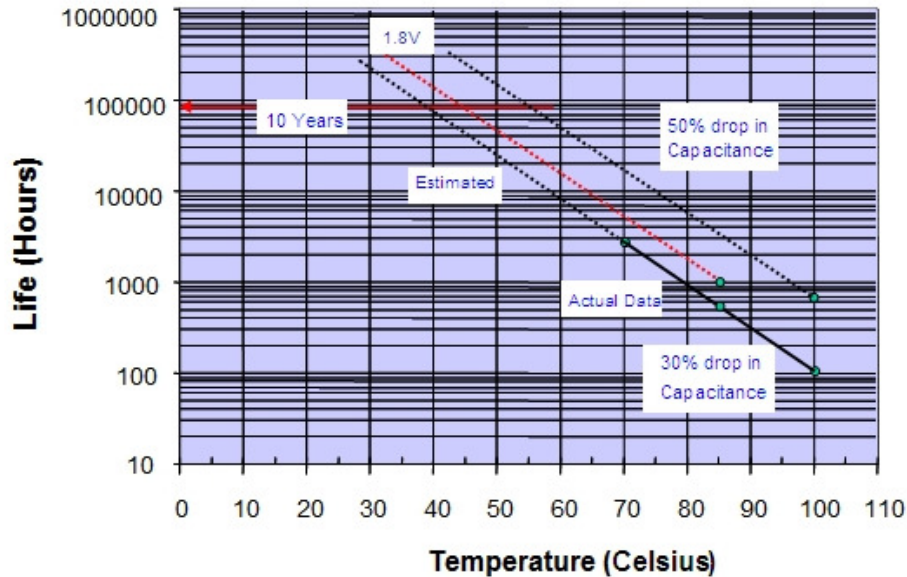
Percent ESR Change
Over Temperature Range



Temperature - C

Additional Selection Criteria

Operating Life:



Additional Selection Criteria

Operating Life:

Average temperature < 40 °C, maximum temperature < 70 °C :

Capacitance Change = -30%

ESR Change = +100% (ESR will be 200% of initial value)

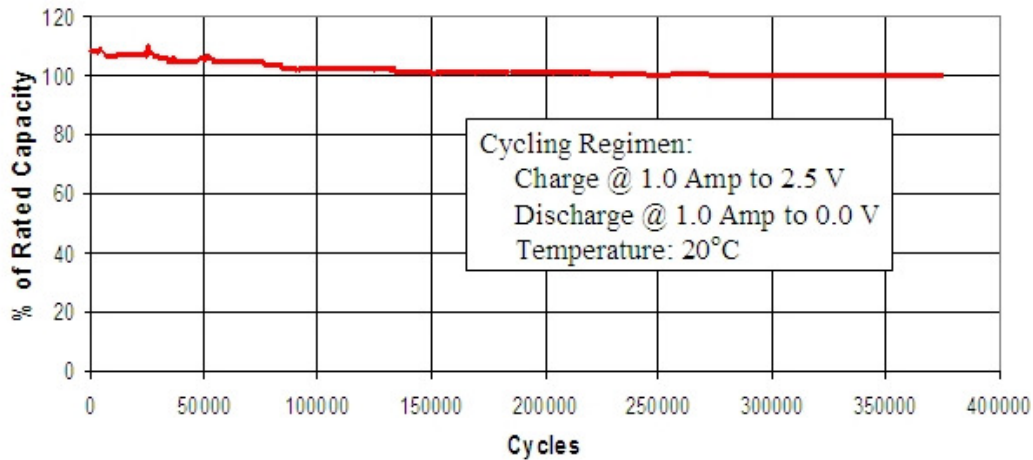
Average temperature > 40 °C, long term exposure to high temperatures,
> 10 year operating life:

Capacitance Change = -50%

ESR Change = +200% (ESR will be 300% of initial value)

Additional Selection Criteria

Operating Life:



Final Product Selection

Adding a requirement for $-10\text{ }^{\circ}\text{C}$ to $+65\text{ }^{\circ}\text{C}$ operation and > 5 years operating life to our example and the required capacitance and ESR is as follows:

For $-10\text{ }^{\circ}\text{C}$ operation:

Required Capacitance = $5\text{F} / 0.85 = 5.88\text{F}$ (drops by 15% @ $-10\text{ }^{\circ}\text{C}$)

ESR Change = $1\text{ Ohm} / 1.60 = 0.625\text{ Ohm}$ (increases by 60% @ $-10\text{ }^{\circ}\text{C}$)

Allowing for > 5 year life:

Required Capacitance = $5.88\text{F} / 0.7 = 8.4\text{F}$ (drops by 30% @ EOL)

ESR Change = $0.625\text{ Ohms} / 2 = 0.312\text{ Ohms}$ (increases by 100% @ EOL)

So we need a part with a specification of $>8.4\text{F}$ and $<0.312\text{ Ohms}$.

Final Product Selection

Selecting a 10F, 0.06 Ohm part, adjusting this for -10 °C operation, end of life and DC discharge gives us:

$$\text{Capacitance} = 10\text{F} \times 0.85 \times 0.7 = 5.95\text{F}$$

$$\text{ESR} = 0.06 \text{ Ohms} \times 1.5 \times 1.6 \times 2 = 0.288 \text{ Ohms}$$

Checking the voltage drop for these values:

$$= i \cdot (R + t/C) = 0.5\text{A} \times (0.288\Omega + 5 \text{ s} / 5.95 \text{ F}) = 0.56\text{V}$$

Voltage drop is too high.

Using two 6.8F, 0.1 Ohm parts connected in parallel:

$$\text{Capacitance} = 13.6\text{F} \times 0.85 \times 0.7 = 8.09\text{F}$$

$$\text{ESR} = 0.05 \text{ Ohms} \times 1.5 \times 1.6 \times 2 = 0.24 \text{ Ohms}$$

$$\text{Voltage Drop} = i \cdot (R + t/C) = 0.5\text{A} \times (0.24\Omega + 5 \text{ s} / 8.09 \text{ F}) = 0.43\text{V}$$

Series Connection of Supercapacitors

For circuits that are required to operation at greater than 2.5V supercapacitors can be connected in series.

Series connection:

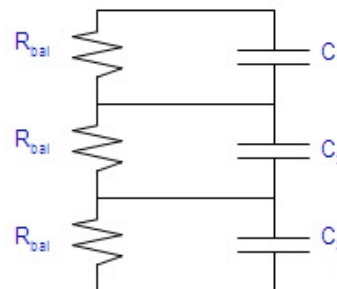
$$C = 1/(1/C_1 + 1/C_2 + 1/C_3)$$

$$\text{ESR} = \text{ESR}_1 + \text{ESR}_2 + \text{ESR}_3$$

Parallel connection:

$$C = C_1 + C_2 + C_3$$

$$\text{ESR} = 1/(1/\text{ESR}_1 + 1/\text{ESR}_2 + 1/\text{ESR}_3)$$



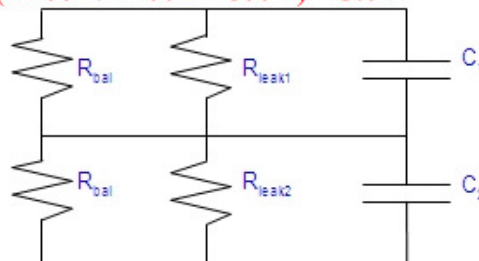
Voltage Balancing

Passive:

$$V_{C1} = V_{\text{supply}} \times R_{\text{leak1}} / (R_{\text{leak1}} + R_{\text{leak2}})$$

Assuming a 5V supply, R_{leak1} equivalent to 1.2 M Ω and R_{leak2} to 800 k Ω then without the addition of balancing resistors, R_{bal} , the voltage on capacitor C_1 would be:

$$V_{C1} = 5V \times (1200k / 1200k + 800k) = 3.0V$$



Voltage Balancing

Passive:

Adding 100 k Ω balancing resistors across each capacitor and the effective leakage resistance values become:

$$\begin{aligned} R_{\text{leak1}}(\text{effective}) &= R_{\text{leak1}} \times R_{\text{bal}} / R_{\text{leak1}} + R_{\text{bal}} \\ &= 1200k \times 100k / 1200k + 100k = 92.31 \text{ k}\Omega \end{aligned}$$

$$\begin{aligned} R_{\text{leak2}}(\text{effective}) &= R_{\text{leak2}} \times R_{\text{bal}} / R_{\text{leak2}} + R_{\text{bal}} \\ &= 800k \times 100k / 800k + 100k = 88.89 \text{ k}\Omega \end{aligned}$$

As a result:

$$V_{C1} = 5V \times (92.31k / 92.31k + 88.89k) = 2.55V$$

Voltage Balancing

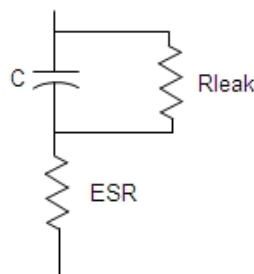
Active:

Advantages of active voltage balancing,

- Effective against imbalance caused by either capacitance or leakage current mismatch
- Rapid voltage balancing can be achieved
- Voltage balancing is very accurate
- Adds only a small amount of additional leakage current

Inflow Current

Inflow current is a combination of charge current and leakage current. Leakage current is a parasitic element that occurs due to supercapacitor construction, this is modelled as a parallel connected resistor.

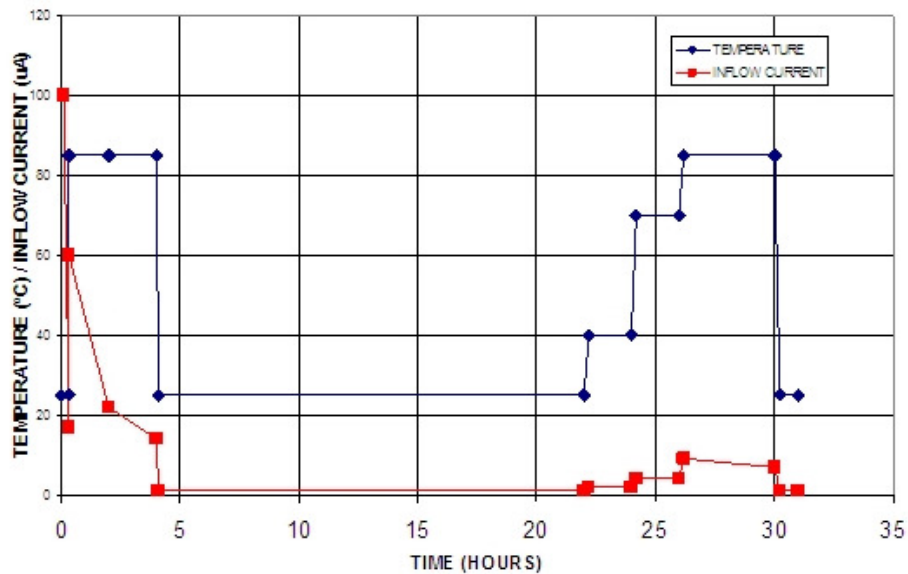


Inflow Current

Inflow current expressed in micro Amps/Farad

Capacitance (F)	100 Hours Charge		1000 Hours Charge	
	25 °C	70 °C	25 °C	70 °C
0.22 – 1.0	3.0 – 6.0	15 – 25	0.5 – 1.5	5 – 10
2.2 – 10	1.5 – 3.0	8 – 15	0.2 – 0.75	3 – 5
22 - 100	1.0 – 2.0	5 - 10	0.1 – 0.5	2 - 4

Inflow Current vs. Temperature



Summary

- Only four basic parameters are required for basic supercapacitor selection
- Allowance needs to be made for changes in capacitance, ESR and leakage current over the operating temperature range
- Apply “rule of thumb” to obtain end of life requirements
- Don't forget the potential effect of leakage current on battery life and capacitor discharge time.
- If in doubt use the PowerStor calculator spreadsheet or contact Cooper Bussmann